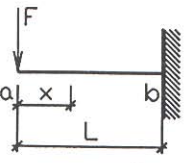
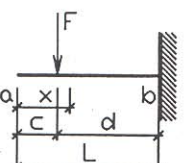
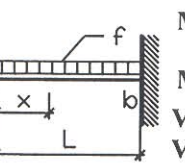
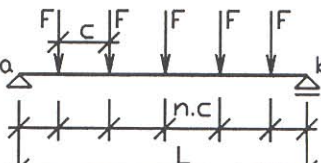
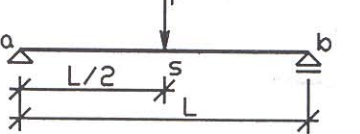
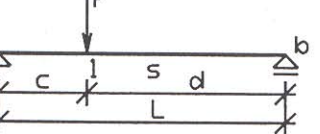
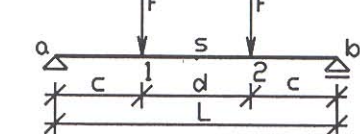
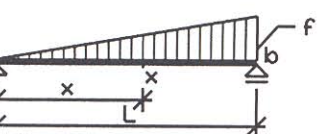
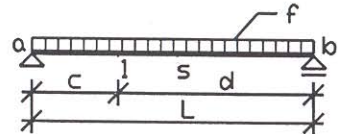
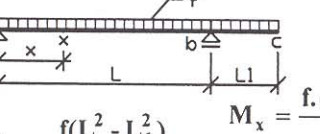
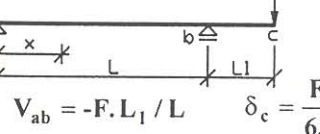
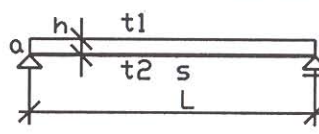
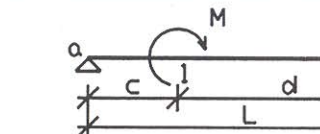
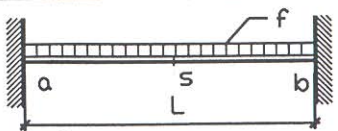
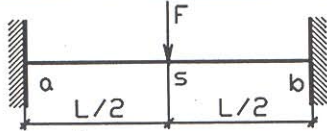
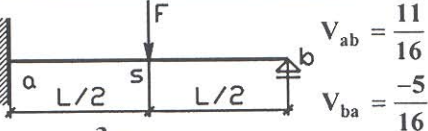
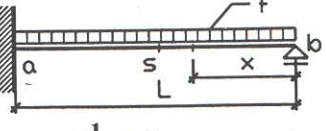
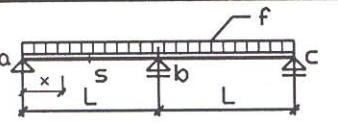
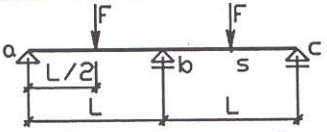
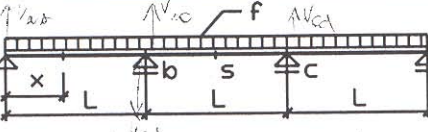
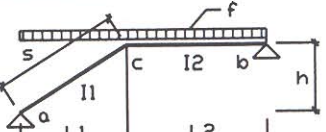
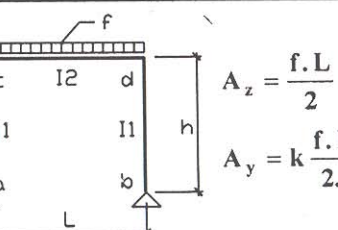
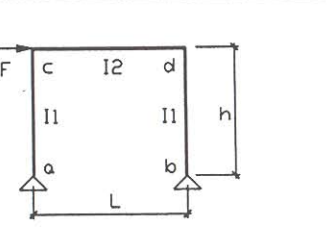
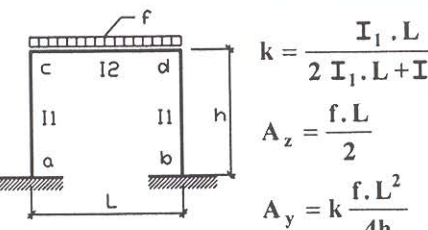
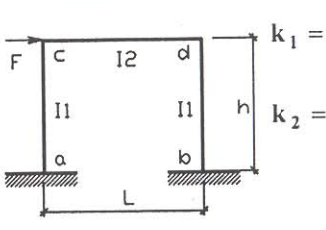


16 Ohybové momenty (M), reakce, posouvající síly (V), průhyby (δ), natočení (α), zatěžovací členy do třímomentových rovnic (N) a náhradní rovnoměrné zatížení (f<sub>c</sub>) na konzole a prostém nosníku pro základní případy zatížení

 $M_b = -F \cdot L$ $M_x = -F \cdot x$ $V_b = -F$ $V_x = -F$ $\delta_a = \frac{F \cdot L^3}{3 E \cdot I}$ $\alpha = \frac{F \cdot L^2}{2 E \cdot I}$	 $M_b = -F \cdot d$ $M_x = -F \cdot (x - c)$ <p>(pro <math>x &lt; c</math> je <math>M_x = 0</math>)</p> $V_b = V_x = -F$ <p>(pro <math>x &lt; c</math> je <math>V_x = 0</math>)</p> $\delta_a = \frac{F \cdot d^2 \cdot (3 \cdot L - d)}{6 E \cdot I}$	 $M_b = -\frac{1}{2} f \cdot L^2$ $M_x = -0,5 f \cdot x^2$ $V_b = -f \cdot L$ $V_x = -f \cdot x$ $\delta_a = \frac{f \cdot L^4}{8 E \cdot I}$ $\alpha = \frac{f \cdot L^3}{6 E \cdot I}$	 $f_c = \frac{n^2 - 1}{n} \cdot \frac{F}{L}$ $V_{ab} = -V_{ba} = \frac{n-1}{2} F$ <p>n - liché: <math>M_s = \frac{n^2 - 1}{8 \cdot n} \cdot F \cdot L</math>    n - sudé: <math>M_s = \frac{n}{8} \cdot F \cdot L</math></p>
 $M_s = \frac{F \cdot L}{4}$ $f_c = \frac{3 \cdot F}{2 \cdot L}$ $V_{ab} = -V_{ba} = \frac{F}{2}$ $\delta_s = \frac{F \cdot L^3}{48 E \cdot I}$ $N_a = N_b = \frac{3}{8} F \cdot L^3$ $\alpha = \frac{F \cdot L^2}{16 E \cdot I}$	 $V_{ab} = \frac{F \cdot d}{L}$ $V_{ba} = -\frac{F \cdot c}{L}$ $M_1 = \frac{F \cdot c \cdot d}{L}$ $\delta_1 = \frac{F \cdot c^2 \cdot d^2}{3 E \cdot I \cdot L}$ $N_a = F \cdot c \cdot d \cdot (L + c)$ $N_b = F \cdot c \cdot d \cdot (L + d)$ <p>pro <math>c \leq L/2</math>: <math>\delta_s = \frac{F c (3 L^2 - 4 c^2)}{48 E I}</math></p>	 $M_1 = M_s = F c$ $N_a = N_b = 3 F c (L - c)$ $V_{ab} = -V_{ba} = F$ $\delta_s = \frac{F c (3 L^2 - 4 c^2)}{24 E I}$ <p>pro <math>c = d = L/3</math>: <math>M_1 = M_2 = M_s = \frac{F \cdot L}{3}</math></p> $\delta_s = \frac{23 \cdot F \cdot L^3}{648 \cdot E \cdot I}$ $N_a = N_b = \frac{2}{3} F \cdot L^3$	 $V_{ab} = -\frac{f \cdot L}{6}$ $V_{ba} = \frac{f \cdot L}{3}$ $M_{x, \max} = \frac{f \cdot L^2}{9 \sqrt{3}}$ $\delta_{\max} = 0,00652 \cdot \frac{f \cdot L^4}{E \cdot I}$ $x_M \cong 0,577 \cdot L$ $x_\delta \cong 0,519 \cdot L$ $N_a = \frac{2 \cdot f \cdot L^4}{15}$ $N_b = \frac{7 \cdot f \cdot L^4}{60}$
 $M_1 = \frac{f c d}{2}$ $M_s = \frac{1}{8} f \cdot L^2$ $V_{ab} = -V_{ba} = \frac{f \cdot L}{2}$ $\delta_s = \frac{5 \cdot f \cdot L^4}{384 \cdot E \cdot I}$ $N_a = N_b = \frac{f \cdot L^4}{4}$ $\alpha = \frac{f \cdot L^3}{24 E \cdot I}$	 $x = \frac{L}{2} \left( 1 - \frac{L_1^2}{L^2} \right)$ $M_x = \frac{f \cdot (L + L_1)^2 (L - L_1)^2}{8 \cdot L^2}$ $V_{ab} = \frac{f(L^2 - L_1^2)}{2 \cdot L}$ $\delta_c = \frac{f \cdot L_1}{24 \cdot E \cdot I} (4L_1^2 \cdot L - L^3 + 3L_1^3)$  $M_x = \frac{-F \cdot L_1 \cdot x}{L}$ $V_{ab} = -F \cdot L_1 / L$ $\delta_c = \frac{F \cdot L_1}{6 \cdot E \cdot I} (2L_1 \cdot L + 2L_1^2)$	 <p>Vliv nerovnoměrného oteplení</p> $M = 0$ $V_{ab} = V_{ba} = 0$ $\delta_s = \frac{\varepsilon \cdot \Delta t^\circ \cdot L^2}{8 \cdot h}$ $\Delta t^\circ = t_2^\circ - t_1^\circ$ $N_a = N_b = \frac{3 \cdot \varepsilon \cdot \Delta t^\circ \cdot E \cdot I \cdot L^2}{h}$	 $M_{1a} = \frac{-M \cdot c}{L}$ $M_{1b} = \frac{M \cdot d}{L}$ $N_a = M(L^2 - 3c^2)$ $V_{ab} = -V_{ba} = \frac{-M}{L}$ <p>pro <math>c = L/2</math> je <math>\delta_1 = 0</math></p> $N_b = M(3d^2 - L^2)$

17 Ohybové momenty (M), reakce, posouvající síly (V), průhyby ( $\delta$ ),  
na vetknutém a spojitým nosníku a jednoduchém rámu pro základní případy zatížení

 $M_a = -\frac{1}{12} f \cdot L^2$ $M_s = \frac{1}{24} f \cdot L^2 \quad \delta_s = \frac{f \cdot L^4}{384 \cdot E \cdot I}$	 $M_a = -\frac{1}{8} F \cdot L$ $M_s = \frac{1}{8} F \cdot L \quad \delta_s = \frac{F \cdot L^3}{192 \cdot E \cdot I}$	 $M_a = -\frac{3}{16} F \cdot L$ $\delta_s = \frac{7 \cdot F \cdot L^3}{768 \cdot E \cdot I}$ $V_{ab} = \frac{11}{16} F$ $V_{ba} = -\frac{5}{16} F$ $M_b = 0$ $M_s = \frac{5}{32} F \cdot L$	 $M_a = -\frac{1}{8} f \cdot L^2$ $\delta_s = \frac{f \cdot L^4}{192 \cdot E \cdot I}$ $M_b = 0$ $M_s = \frac{1}{16} f \cdot L^2$ $M_x = \frac{9}{128} f \cdot L^2$ $V_{ab} = \frac{5}{8} f \cdot L$ $V_{ba} = -\frac{3}{8} f \cdot L$ $x = \frac{3}{8} L$
 $M_b = -\frac{1}{8} f \cdot L^2$ $M_s = \frac{1}{16} f \cdot L^2$ $x = \frac{3}{8} L$ $M_x = \frac{9}{128} f \cdot L^2$ $V_{ab} = A = \frac{3}{8} f \cdot L$ $V_{bc} = \frac{5}{8} f \cdot L$ $B = \frac{10}{8} f \cdot L$ $\delta_x \cong \frac{f \cdot L^4}{190 \cdot E \cdot I}$	 $M_b = -\frac{3}{16} F \cdot L$ $M_s = \frac{5}{32} F \cdot L$ $V_{ab} = A = \frac{5}{16} F$ $V_{bc} = \frac{11}{16} F$ $B = \frac{11}{8} F$ $\delta_s = \frac{7 \cdot F \cdot L^3}{768 \cdot E \cdot I}$	 $M_b = -\frac{1}{10} f \cdot L^2$ $M_s = \frac{1}{40} f \cdot L^2$ $x = \frac{2}{5} L$ $M_x = \frac{2}{25} f \cdot L^2$ $V_{ab} = A = \frac{2}{5} f \cdot L$ $V_{cd} = \frac{3}{5} f \cdot L$ $B = \frac{11}{10} f \cdot L$ $V_{bc} = \frac{1}{2} f \cdot L$	 $M_c = k_1 \frac{-f \cdot L_2^2}{8}$ $A_y = B_y = \frac{f \cdot L_2}{8h} (4L_1 + k_1 \cdot L_2)$ $A_z = \frac{f \cdot L_2}{8} (5k_1 + 4k_2) \quad k_1 = \frac{I_1 \cdot L_2}{I_1 \cdot L_2 + I_2 \cdot s}$ $B_z = \frac{f \cdot L_2}{8} (3k_1 + 4k_2) \quad k_2 = \frac{I_2 \cdot s}{I_1 \cdot L_2 + I_2 \cdot s}$
 $A_z = \frac{f \cdot L}{2}$ $A_y = k \frac{f \cdot L^2}{2 \cdot h}$ $k = \frac{I_1 \cdot L}{6 I_1 \cdot L + 4 h \cdot I_2}$ $M_c = M_d = k \frac{-f \cdot L^2}{2}$	 $M_c = -M_d = \frac{F \cdot h}{2}$ $A_z = -B_z = \frac{F \cdot h}{L} \quad A_y = B_y = \frac{F}{2}$	 $k = \frac{I_1 \cdot L}{2 I_1 \cdot L + I_2 \cdot h}$ $A_z = \frac{f \cdot L}{2}$ $A_y = k \frac{f \cdot L^2}{4h}$ $M_a = M_b = k \frac{f \cdot L^2}{12}$ $M_c = M_d = k \frac{-f \cdot L^2}{6}$	 $k_1 = \frac{I_2 \cdot h}{I_1 \cdot L + 6 I_2 \cdot h}$ $k_2 = \frac{I_1 \cdot L + 3 I_2 \cdot h}{I_1 \cdot L + 6 I_2 \cdot h}$ $M_a = -M_b = k_2 \frac{-F \cdot h}{2}$ $M_c = -M_d = k_1 \frac{3 F \cdot h}{2}$ $A_z = -B_z = k_1 \frac{-3 F \cdot h}{L}$ $A_y = B_y = \frac{F}{2}$

DEFORMACE PROSTÉHO NOSNÍKU KONSTANTNÍHO PRŮŘEZU

	ZATÍŽENÍ	PRŮHYB $y$ $y_{max} = f$	POOTOČENÍ PODPOROVÝCH PRŮŘEZŮ
1		$f = \frac{Pab}{27EJl} \sqrt{3a(l+b)^3}$ $v x = \sqrt{\frac{2}{3}} a(l+b)$	$\varphi_a = \frac{Pb}{6EJl} (l^2 - b^2)$ $\varphi_b = \frac{Pa}{6EJl} (l^2 - a^2)$
2		$f = \frac{Pl^3}{48EJ} \quad v x = 0,5l$	$\varphi_a = \varphi_b = \frac{Pl^2}{16EJ}$
3		$f = \frac{Pl^3}{28,17EJ} \quad v x = 0,5l$	$\varphi_a = \varphi_b = \frac{Pl^2}{9EJ}$
4		$f = \frac{Pl^3}{20,22EJ} \quad v x = 0,5l$	$\varphi_a = \varphi_b = \frac{5}{32} \frac{Pl^2}{EJ}$
5		$f = \frac{Pl^3}{15,73EJ} \quad v x = 0,5l$	$\varphi_a = \varphi_b = \frac{1}{5} \frac{Pl^2}{EJ}$
6		$f = \frac{Pl^3}{13,05EJ} \quad v x = 0,5l$	$\varphi_a = \varphi_b = \frac{35}{144} \frac{Pl^2}{EJ}$
7		$f = \frac{Pl^3}{24EJ} (3\frac{a}{l} - 4\frac{a^3}{l^3})$ $v x = 0,5l$	$\varphi_a = \varphi_b = \frac{Pa}{2EJ} (l - a)$
8		$f = \frac{11}{384} \frac{Pl^3}{EJ} \quad v x = 0,5l$	$\varphi_a = \varphi_b = \frac{3}{32} \frac{Pl^2}{EJ}$
9		$f = \frac{Pl^3}{24,45EJ} \quad v x = 0,5l$	$\varphi_a = \varphi_b = \frac{19}{144} \frac{Pl^2}{EJ}$
10		$f = \frac{Pl^3}{19,04EJ} \quad v x = 0,5l$	$\varphi_a = \varphi_b = \frac{33}{192} \frac{Pl^2}{EJ}$
11		$f = \frac{Pl^3}{15,1EJ} \quad v x = 0,5l$	$\varphi_a = \varphi_b = \frac{51}{240} \frac{Pl^2}{EJ}$
12		$y = \frac{qa^2b}{24EJ} (4 - 3\frac{a}{l})$ $v x = a$	$\varphi_a = \frac{qa^2c}{6EJ} (1 - \frac{a}{2l})^2$ $\varphi_b = \frac{qa^2c}{12EJ} (1 - \frac{a^2}{2l^2})$
13		$y = \frac{qc}{6EJ} [ \frac{ab}{l} (2a^2 - 2a^2 - \frac{a^3}{l}) + \frac{c^3}{6l} ] \quad v x = a$	$\varphi_a = \frac{q}{24EJ} \frac{bc}{l} [4a(l+b) - c^2]$ $\varphi_b = \frac{q}{24EJ} \frac{ac}{l} [4b(l+a) - c^2]$

	ZATÍŽENÍ	MAXIMÁLNÍ PRŮHYB $f$	POOTOČENÍ PODPOROVÝCH PRŮŘEZŮ
14		$f = \frac{qL^2}{48EJ} \frac{a^2}{l^2} (3 - 2\frac{a}{l^2})$ $v x = 0,5l$	$\varphi_a = \varphi_b = \frac{qa^2}{12EJ} (3l - 2a)$
15		$f = \frac{5}{384} \frac{qL^4}{EJ} \quad v x = 0,5l$	$\varphi_a = \varphi_b = \frac{1}{24} \frac{qL^3}{EJ}$
16		$y = \frac{2a^2c}{45EJ} (5 - 9\frac{a}{l} + 4\frac{a^2}{l^2})$ $v x = a$	$\varphi_a = \frac{2a^2c}{360EJ} (40 - 45\frac{a}{l} + 12\frac{a^2}{l^2})$ $\varphi_b = \frac{2a^2c}{360EJ} (5 - 3\frac{a^2}{l^2})$
17		$y = \frac{qa^2bl}{360EJ} (20\frac{c}{l} - 13\frac{a^2}{l^2})$ $v x = a$	$\varphi_a = \frac{9c^2a}{360EJ} (20 - 15\frac{a}{l} + 3\frac{a^2}{l^2})$ $\varphi_b = \frac{9c^2a}{360EJ} (10 - 3\frac{a^2}{l^2})$
18		$f = 0,00652 \frac{qL^4}{EJ}$ $v x = 0,519l$	$\varphi_a = \frac{7}{360} \frac{qL^3}{EJ}$ $\varphi_b = \frac{8}{360} \frac{qL^3}{EJ}$
19		$f = \frac{1}{120} \frac{qL^4}{EJ} \quad v x = 0,5l$	$\varphi_a = \varphi_b = \frac{5}{192} \frac{qL^3}{EJ}$
20		$f = \frac{3}{840} \frac{qL^4}{EJ} \quad v x = 0,5l$	$\varphi_a = \varphi_b = \frac{1}{84} \frac{qL^3}{EJ}$
21		$f = \frac{7}{1024} \frac{qL^4}{EJ} \quad v x = 0,5l$	$\varphi_a = \varphi_b = \frac{7}{768} \frac{qL^3}{EJ}$
22		$f = \frac{19}{3072} \frac{qL^4}{EJ} \quad v x = 0,5l$	$\varphi_a = \varphi_b = \frac{5}{256} \frac{qL^3}{EJ}$
23		$f = \frac{5}{384} \frac{qL^4}{EJ} (1 - \frac{8}{3}\frac{a^2}{l^2} + \frac{16}{25}\frac{a^4}{l^4})$ $v x = 0,5l$	$\varphi_a = \varphi_b = \frac{qL^3}{24EJ} (1 - 2\frac{a^2}{l^2} + \frac{a^4}{l^4})$
24		$f = 0,0065 (q_a + q_b) l^4$ $v x \propto 0,5l$ do $0,519l$	$\varphi_a = \frac{q^3}{360EJ} (8q_a + 7q_b)$ $\varphi_b = \frac{q^3}{360EJ} (7q_a + 8q_b)$
25		$y = \frac{Mab}{3EJ} \frac{a-b}{l}$ $v x = a$	$\varphi_a = \frac{Ml}{6EJ} (1 - 3\frac{a^2}{l^2})$ $\varphi_b = \frac{Ml}{6EJ} (1 - 3\frac{a^2}{l^2})$
26		$f = \frac{Ml^2}{15,59EJ} = 0,0642 \frac{Ml^2}{EJ}$ $v x = 0,423l$	$\varphi_a = \frac{Ml}{3EJ} \quad \varphi_b = \frac{Ml}{6EJ}$

Tabulka C.72. Lichoběžníkový portálový rám kloubově uložený

	$k_1 = \frac{I_1}{s}$	$k_2 = \frac{I_2}{b}$	$N = 3k_1 + 2k_2$
Způsob zatížení	Průběh momentů		
	$H = \frac{g}{4h} \frac{6a(a+b)k_1 + b^2k_1 + a(5a+4b)k_2}{N}$ $M_c = M_d = \frac{1}{2}ga(a+b) - Hh$ $M_s = \frac{1}{8}gl^2 - Hh$ $A = B = \frac{1}{2}gl$		
	$H = \frac{gb}{4hN} [bk_1 + 2a(3k_1 + 2k_2)]$ $M_c = M_d = Aa - Hh$ $A = B = \frac{1}{2}gb$		
	$H = \frac{gh}{8N} (6k_1 + 5k_2)$ $M_c = B(l-a) - Hh$ $M_d = Ba - Hh$ $A = -\frac{gh^2}{2l} \quad B = -A$		
	$H = \frac{P}{2hbN} [3(cd - a^2)k_1 + 2abk_2]$ $M_c = Aa - Hh \quad M_p = Ac - Hh$ $M_d = Ba - Hh$ $A = \frac{Pd}{l} \quad B = \frac{Pc}{l}$		
	$H = \frac{Pc}{2hN} \left[ 3k_1 + \left( 3 - \frac{c^2}{h^2} \right) k_2 \right]$ $M_p = P_c \left[ 1 - \frac{ac}{hl} \right] - Hc$ $M_c = B(l-a) - Hh$ $M_d = Ba - Hh$ $A = -\frac{Pc}{l} \quad B = -A$		

Tabulka C.73. Jednoduchý obdélníkový rám kloubově uložený

	$k_1 = \frac{I_1}{h}$	$k_2 = \frac{I_2}{l}$	$N = 2(3k_1 + 2k_2)$
Způsob zatížení	Průběh momentů		
	$H = \frac{gl^2 k_1}{2h N}$ $M_c = M_d = -\frac{gl^2 k_1}{2 N}$		
	$H = \frac{gh}{4} \frac{6k_1 + 5k_2}{N}$ $M_c = \frac{3gh^2}{4} \frac{2k_1 + k_2}{N}$ $M_d = -\frac{gh^2}{4} \frac{6k_1 + 5k_2}{N}$		
	$H = \frac{3Pab k_1}{hl N}$ $M_c = M_d = -\frac{3Pab k_1}{l N}$		
	$H = \frac{3Pl k_1}{4h N}$ $M_c = M_d = -\frac{3Pl k_1}{4 N}$		
	$H = \frac{Pa}{h^2} \frac{3h^2 k_1 + (3h^2 - a^2) k_2}{N}$ $M_c = \frac{Pa}{h^2} \frac{3h^2 k_1 + (a^2 + h^2) k_2}{N}$ $M_d = -\frac{Pa}{h^2} \frac{3h^2 k_1 + (3h^2 - a^2) k_2}{N}$		
	$H = \frac{P}{2}$ $M_c = \frac{Ph}{2} \quad M_d = -\frac{Ph}{2}$		
	$H = -\frac{3Pa k_1}{h N}$ <p>Na sloupech:</p> $M_c = M_d = \frac{3Pak_1}{N}$		

Tabulka C.77. Jednoduchý obdélníkový rám dokonale vetknutý

$$k_1 = \frac{I_1}{h} \quad k_2 = \frac{I_2}{l} \quad L = k_1 + 6k_2 \quad N = (k_1 + 6k_2)(2k_1 + k_2) \quad R = 2k_1 + k_2$$

Způsob zatížení	Průběh momentů	Statické veličiny
		$H = \frac{gl^2 k_1}{4h R}$ $M_o = M_b = \frac{gl^2 k_1}{12 R}$ $M_c = M_d = -\frac{gl^2 k_1}{6 R}$
		$H = \frac{gh}{8N} (3k_1^2 + 20k_1 k_2 + 12k_2^2)$ $M_o = -\frac{gh^2}{24N} (15k_1^2 + 73k_1 k_2 + 30k_2^2)$ $M_b = \frac{gh^2}{24N} (9k_1^2 + 35k_1 k_2 + 18k_2^2)$ $M_c = \frac{gh^2 k_2}{24N} (23k_1 + 6k_2) \quad M_d = -\frac{gh^2 k_2}{24N} (25k_1 + 18k_2)$
		$\alpha = 1 + \frac{a(b-a)k_1}{Ll^2} \quad \beta = 1 - \frac{b(b-a)k_1}{Ll^2}$ $H = \frac{3Pab k_1}{2hl R} \quad M_o = \frac{Pabk_1}{2l^2 N} [(3k_1 + 7k_2)a + (5k_2 - k_1)b]$ $M_b = \frac{Pabk_1}{2l^2 N} [(5k_2 - k_1)a + (3k_1 + 7k_2)b]$ $M_c = -\frac{Pabk_1}{2l^2 N} [11ak_2 + (4k_1 + 13k_2)b]$ $M_d = -\frac{Pabk_1}{2l^2 N} [(4k_1 + 13k_2)a + 11bk_2]$
		$H = \frac{3Pl k_1}{8h R}$ $M_o = M_b = \frac{Pl k_1}{8 R}$ $M_c = M_d = -\frac{Pl k_1}{4 R}$
		$H = \frac{P}{2}$ $M_o = -M_b = -\frac{Ph k_1 + 3k_2}{2 L}$ $M_c = -M_d = \frac{3Ph k_2}{2 L}$

pokračování tab. C.77

Způsob zatížení	Průběh momentů	Statické veličiny
		$H = \frac{Pc}{h} \left[ 1 + \frac{b(2h-3b)}{h^2} + \frac{a(2h-3a)k_2 - k_1}{h^2 R} \right]$ $M_o = M_b = \frac{Pc}{h^2} \left[ b(2h-3b) - \frac{a(2h-3a)k_1}{R} \right]$ $M_c = M_d = \frac{Pac(2h-3a)k_2}{h^2 R}$
		$H = \frac{ph}{40R} (4k_1 + 3k_2)$ $M_o = -\frac{ph^2}{120N} (28k_1^2 + 151k_1 k_2 + 63k_2^2)$ $M_b = \frac{ph^2}{120N} (12k_1^2 + 49k_1 k_2 + 27k_2^2)$ $M_c = \frac{ph^2 k_2}{120N} (28k_1 + 3k_2) \quad M_d = -\frac{ph^2 k_2}{120N} (32k_1 + 27k_2)$
		$H = -\frac{3M k_1}{2h R}$ $M_o = -\frac{Mk_1}{2N} (5k_2 - k_1) \quad M_b = -\frac{Mk_1}{2N} (3k_1 + 7k_2)$ <p>Na sloupech: <math>M_c = \frac{Mk_1}{2N} (4k_1 + 13k_2)</math></p> $M_d = \frac{11Mk_1 k_2}{2N}$ <p>Na trámu: <math>M_e = -\frac{Mk_2}{2N} (13k_1 + 12k_2)</math></p>
		$H = \frac{3E\alpha t l}{h^2(1 + \alpha t)} \frac{(k_1 + 2k_2)k_1}{R}$ $M_o = M_b = \frac{3E\alpha t l k_1}{h(1 + \alpha t)} \frac{k_1 + k_2}{R}$ $M_c = M_d = -\frac{3E\alpha t l}{h(1 + \alpha t)} \frac{k_1 k_2}{R}$

Podrobněji viz O. Novák: Jednoduchý rám ve vzorcích. Praha, SNTL 1967.